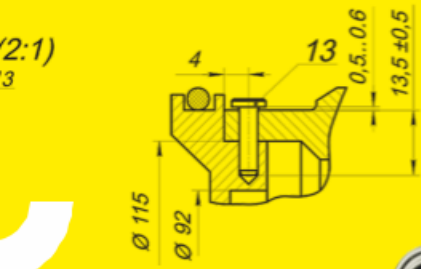


# ROLLING BEARINGS

Fits



2 WHEELERS 3 WHEELERS 4 WHEELERS TRACTORS



LCV, HCV INDUSTRIES RAILWAYS



## About National Engineering Industries Ltd. (NBC Bearings)

A symbol of dependability and flexible engineering solutions, NBC Bearings is the brand of National Engineering Industries. Founded in 1946, National Engineering Industries Ltd (NEI) is India's leading bearings manufacturer and exporter, renowned for excellence in quality and delivery. In 2021, NBC bearings completed 75 years of its incorporation.

Headquartered in Jaipur, Having started with 30,000 bearings in 19 sizes in 1946, NBC has evolved to manufacture over 200 million bearings each year offering in 2300+ variants to serve a host of customers in India and over 30 other countries across five continents in automotive, railways and industrial segments. NBC also serves the Indian aftermarket through a countrywide network of 550+ authorized stockists and thousands of retailers.

### Award & Recognitions :

NBC has been the recipient of several award and accolades for its quality consciousness and manufacturing prowess. Most prominent being the coveted Deming Grand Prize which is the highest honour in quality awarded to a company for excellence in Total Quality Management (TQM). NBC bearings is the only bearing manufacturer to win both - The Deming Application Award and The Deming Grand Prize Award.

The award is given by the Japanese Union of Scientists and Engineers (JUSE) to companies for demonstrating practicing TQM in the areas of production, customer service, safety, human resource, corporate social responsibility, environment, etc. NBC stands committed to an endless journey of continuous improvement through TQM.

# Fits

## 10.1 The Necessity of a Proper Fit

In some cases improper fit may lead to damage and shorten bearing life. Therefore, it is necessary to make a careful analysis while selecting a proper fit.

Some of the negative conditions caused by improper fit are listed below:

- Raceway cracking, early pitting and displacement of raceways
- Raceway & shaft or housing abrasion caused by creeping in fretting corrosion
- Seizing caused by loss of internal clearance
- Increased noise & lowered rotational accuracy due to raceway groove deformation.

**Selection of fits** : Selection of proper fit depended upon thorough analysis of bearing operating conditions, including consideration of following factors:

### (1) Condition of Rotation

This condition refer to the rotation of bearing ring being considered in relation to the direction of load. There are 3 different conditions:

- Rotating load
- Stationery load
- Direction of load indeterminate

### (2) Magnitude of the load

The interference fit of a bearing's inner ring on its seating will be loosened with the increasing load, as the ring will expand under the influence of rotating load, & ring may begin to creep. If it is of shock character, greater interference is required.

The loss of interference due to increasing load can be estimated using the following equation:

**When  $Fr \leq 0.3Cor$**

$$\Delta dp = 0.08 \sqrt{\frac{d.Fr}{B}}$$

**When  $Fr \geq 0.3 Cor$**

$$\Delta dp = 0.02 (Fr/B)$$

where,

$\Delta dp$  = Interference decrease of inner ring ( $\mu\text{m}$ )

$Fr$  = Radial load (N)

$B$  = Inner ring width (mm)

$Cor$  = Basic static load (N)

### (3) Bearing Internal Clearance

An interference fit of a bearing on the shaft or in housing means that ring is elastically deformed (expanded or compressed) and bearing's internal clearance reduced.

The internal clearance and permissible reduction depend on the type and size of the bearing.

- The reduction in clearance due to interference fit can be so large that bearings with an internal clearance which is greater than normal have to be used.
- The expansion of the inner ring and contraction of outer ring can be assumed to be approximately 60-80% of the interference, depending on the material of shaft and housing.

### (4) Temperature Condition

Interference between inner ring & steel shaft is reduced as a result of temperature increase (difference between bearing temperature and ambient temperature). This can result in an easing of fit of the inner ring on its seating. While outer ring expansion may result in increase in clearance.

The decrease of the interference of the inner ring due to this

temperature difference may be calculated using following equation:  $\Delta dt = 0.0015 \times d \times \Delta T$

Where  $\Delta dt$  = effective interference for temperature difference ( $\mu\text{m}$ )

$\Delta T$  = Temperature difference between bearing temperature ambient temperature (deg. C).

$d$  = Bearing bore diameter (mm)

### (5) Running Accuracy Requirement

To reduce resilience and vibration, clearance fit should generally not be used for bearings, where high demands are placed on running accuracy.

### (6) Design & Material of Shaft & Housing

The fit of a bearing ring on its seating must not lead to uneven distortion of the ring (out of roundness). This can be caused by discontinuity in the housing surface. Split housings are therefore not suitable where outer rings are to have an interference fit.

### (7) Ease of Mounting & Dismounting

Bearings with clearance fit are usually easier to mount or dismount than those having interference fit. Where operating condition necessitate interference fit and it is essential that mounting & dismounting can be done easily, separable bearings or bearings with taper bore and adaptor or withdrawal sleeve may be used.

### (8) Displacement of Non-Locating bearings

If non-separable bearings are used as floating bearings, if the ring is under stationary load, so that axial displacement has to take place in the housing bore, a hardened intermediate bushing is often fitted to the outer ring.

### (9) Effective Interference and finish of shaft & housing

Roughness of the fitted surface is reduced since the roughness of the fitted surface is reduced during fitting, the effective interference becomes less than the apparent interference.

The amount of this interference decrease varies depending on roughness of the surfaces.

Normally, manufacturers assume the following interference reductions:

For ground shaft: 1-2.5 Micron

Machined Shaft: 5-7 Micron

### (10) Fitting stress & ring expansion and contraction

While calculating the minimum required amount of interference, following factors should be factors should be taken into consideration:

- Interference is reduced by radial load
- Interference is reduced by difference between bearing temperature and ambient temperature
- Interference is reduced by variation of fitted surfaces

**Important details on fits:** Maximum interference should not exceed the ratio of 1:1000 of shaft or outside diameter.

Tight interference fits are recommended for:

- (a) Operating conditions with large vibrations or shock loads
- (b) Application using hollow shaft of housing with thin walls
- (c) Application using housing made of light alloys or plastic.

Loose interferences are recommended for:

- (a) Application requiring high running accuracy
- (b) Application using small size bearings or thin walled bearings.

Shaft and housing material, geometry, hardness and surface finish must be carefully controlled.

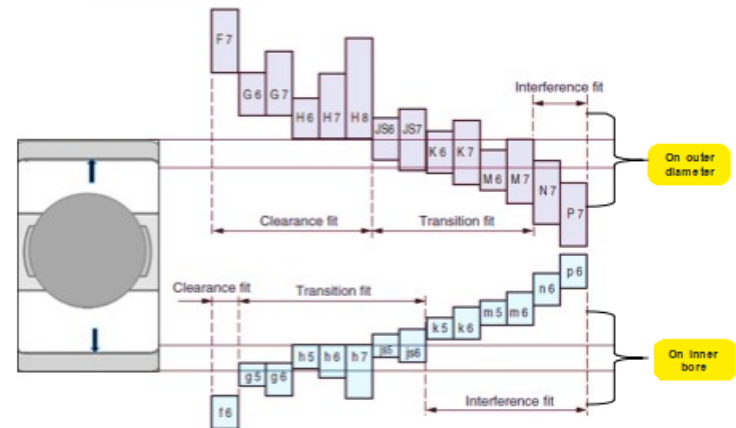
- Ground shafts should be finished to 1.3 micron Ra or better;
- For turned shafts a finish of 2.5 micron Ra or better; and
- Housing bores should be finished to 4 micron Ra or better.

To avoid shearing of aluminum and magnesium housing during bearing installation, steel inserts should be used; alternatively special lubricants may be used for Freezing and heating to facilitate assembly. A minimum interference fit of 0.0015" and 0.001" per inch of diameter is required for magnesium and aluminum housing respectively.

Where bearings are to be pressed onto a hollow shaft, allowance must be made for contraction of the hollow shaft in order to maintain the desired radial pressure.

## 10.2 Housing & Shaft Tolerance Class

NEI engineering department should be consulted for proper fitting practices on all special applications. For normal class bearing shaft and housing tolerances are given in table below. The tolerances are for solid steel shaft & housing of cast iron and steel.



Shaft & Housing tolerances

## Shaft tolerance class generally for radial bearings (classes 0, 6X and 6)

Type of load	Condition	Example	Shaft diameters			
			Ball bearings	Cylindrical roller and tapered roller bearings	Spherical roller bearings	Tolerance class symbol
Rotating inner ring load	Light and variable loads (P<0,06C)	Conveyors lightly loaded mechanisms, bearings	18...100 >100...140	<40 40...100	- -	j6 k6
	Normal and heavy loads (P>0, 06C)	General mechanical engineering electric motors, turbines, pumps, gearboxes,	<18	-	-	j5
			18...100	<40	<40	K5(j6)
			>100...140	40...100	40...65	m5(m6)
			>140...200	>100...140	>65...100	n6
Heavy loads and shock loads, arduous working conditions (P>0, 12C)	Heavy duty railway vehicles axle bearings, traction motors, rolling mills	>200...280	>140...200	>100...140	p6	
		-	>200...400	>140...280	e6	
		-	-	>280...500	k7	
High running accuracy, light loads (P>0,06C)	Machine tools	<18	-	-	h5	
		>18...100	<40	-	j5	
		>100...200	40...100	-	k5	
		-	>140...200	-	m5	
Stationary inner ring load	Radial bearings with cylindrical cone		All diameters			g6(h6)
	Easy axial displacement of inner ring on shaft desirable	Wheels on non-rotating shafts (free wheel)				
	Axial displacement of inner ring on shaft not necessary	Tension pulleys, sheaves				h6
Axial load	Common to all shaft diameter. Shaft & inner is not fixed		<250 >250	<250 >250	<250 >250	j6 j6

## Fits for shaft for Tapered bore bearing (normal class) with adapter / withdrawal sleeve

All loads	For all sizes general applications	All shaft diameters	h9
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## Housing tolerance class generally for radial bearings (classes 0, 6X and 6)

Split or Single (Housing rotating outer ring load)				
Load type	Conditions	Example	Tolerance class	Outer ring axial displacement in non-separable bearing
Rotating outer ring load	Light and variable loads (P<0,06C)	Roller bearing wheel hubs, connecting rod bearing	M7	Outer ring cannot move axially
	Normal and heavy loads (P>0,06C)	Ball bearing wheel hubs, connecting rod bearings, crane traveling wheels	N7	
	Rotating outer ring load Heavy loads on bearings in thin-walled housings, heavy shock loads (P>0,12C)	Conveyor rollers, rope sheaves, belt tension pulleys	P7	
Direction of load indeterminate	Normal and heavy loads (P > 0,06C). Outer ring displacement is not necessary	Crank shaft main bearing	K7	Outer ring cannot move axially
		Electric motors, pumps crankshaft main bearing		
	Heavy shock loads	Traction motors	M7	

Split or Single Housing (Stationary outer load)				
Load type	Conditions	Example	Tolerance class	Outer ring axial displacement in non-separable bearing
Stationary outer load	Loads of all kinds	General mechanical engineering, railway axle boxes	H7	Outer ring can move axially
	Light and normal loads Desirable outer ring displacement (Ps0,12 C)		H8	Outer ring cannot move axially
	Quiet operation		H6	
	Heat conduction through shaft	Drying cylinders, large electrical machines with spherical roller bearings	G7	
Direction of load indeterminate	Light and normal loads Desirable outer ring displacement (Ps0,12 C)	medium-sized electric motors, pumps, crankshaft main bearings	J7	Outer ring can move axially



Numeric value table of fitting for radial bearing of 'Normal class' for metric size

Table for fit on shaft Unit  $\mu\text{m}$

Nominal inside diameter of bearing d (mm)	$\Delta\text{dmp}$	05	06	h5	h6	i5	j5	i6	
									high
3	0	-8	4T-9L	4T-12L	8T-5L	8T-8L	11T-2L	10.5T-2.5L	14T-2L
5	10	-8	3T-11L	3T-14L	8T-9L	8T-9L	12T-2L	11T-3L	15T-2L
10	18	-8	2T-14L	2T-17L	8T-8L	8T-11L	13T-3L	12T-4L	16T-3L
18	30	-10	3T-14L	3T-20L	10T-9L	10T-13L	15T-4L	14.5T-4.5L	19T-4L
30	50	-12	3T-20L	3T-25L	12T-11L	12T-16L	18T-5L	17.5T-5.5L	23T-5L
50	80	-15	5T-23L	5T-29L	15T-13L	15T-19L	21-7L	21.5T-6.5L	27T-7L
80	120	-20	8T-27L	8T-34L	20T-15L	20T-22L	26T-9L	27.5T-7.5L	33T-9L
120	140								
140	160	-25	11T-32L	11T-39L	25T-18L	25T-25L	32T-11L	34T-9L	39T-11L
160	180								
180	200								
200	225	-30	15T-35L	15T-44L	30T-20L	30T-29L	37T-13L	40T-10L	46T-13L
225	250								
250	280								
280	315	-35	18T-40L	18T-49L	35T-23L	35T-32L	42T-16L	46.5T-11.5L	51T-16L
315	355								
355	400	-40	22T-43L	22T-54L	40T-25L	40T-36L	47T-18L	52.5T-12.5L	58T-18L
400	450								
450	500	-45	25T-47L	25T-60L	45T-27L	45T-40L	52T-20L	58.5T-13.5L	65T-20L

Table for fit on Housing Unit  $\mu\text{m}$

Nominal outside diameter of bearing D (mm)	$\Delta\text{Dmp}$	Over	Incl.	high	low							
6	10	0	-8	5L-28L	0-17L	0-23L	4T-13L	7T-16L	7.5-15.5L	7T-10L		
10	18	0	-8	6L-32L	0-19L	0-26L	5T-14L	8T-18L	9T-17L	9T-10L		
18	30	0	-9	7L-37L	0-22L	0-30L	5T-17L	9T-21L	10.5T-19.5L	11T-11L		
30	50	0	-11	9L-45L	0-27L	0-36L	6T-21L	11T-25L	12.5T-23.5L	13T-14L		
50	80	0	-13	10L-53L	0-32L	0-42L	6T-26L	12T-31L	15T-28L	15T-17L		
80	120	0	-15	12L-62L	0-37L	0-50L	6T-31L	13T-37L	17.5T-32.5L	18T-19L		
120	150	0	-18	14L-72L	0-43L	0-58L	7T-36L	14T-44L	20T-38L	21T-22L		
150	180	0	-25	14L-79L	0-50L	0-65L	7T-43L	14T-51L	20T-45L	21T-29L		
180	250	0	-30	15L-91L	0-59L	0-76L	7T-52L	15T-60L	23T-53L	24T-35L		
250	315	0	-35	17L-104	0-67L	0-87L	7T-60L	16T-71L	26T-61L	27T-40L		
315	400	0	-40	18L-115L	0-76L	0-97L	7T-69L	18T-79L	28.5T-68.5L	29T-47L		
400	500	0	-45	20L-128L	0-85L	0-108L	7T-78L	20T-88L	31.5T-76.5L	32T-53L		

Numeric value table of fitting for radial bearing of 'Normal class' for metric size

Table for fit on shaft Unit  $\mu\text{m}$

Nominal inside diameter of bearing d (mm)	$\Delta\text{dmp}$	05	06	h5	h6	m5	m6	n6	p6	r6
3	0	-8	12T-4L	14T-11	17T-11	17T-91	20T-91	24T-8T	28T-12T	-
5	10	-8	12.5T-4.5L	15T-11	18T-11	20T-61	23T-61	27T-10T	32T-15T	-
10	18	-8	13.5T-5.5L	17T-11	20T-11	23T-71	26T-71	31T-12T	37T-18T	-
18	30	-10	16.5T-6.5L	21T-21	25T-21	27T-81	31T-81	38T-15T	45T-22T	-
30	50	-12	20T-8L	25T-21	30T-21	32T-91	37T-91	45T-17T	54T-26T	-
50	80	-15	24.5T-9.5L	30T-21	36T-21	39T-111	45T-111	54T-20T	66T-32T	-
80	120	-20	31T-11L	38T-21	45T-21	48T-131	55T-131	65T-23T	79T-37T	-
120	140									113T-63T
140	160	-25	37.5T-12.5L	46T-21	53T-21	58T-151	65T-151	77T-27T	93T-43T	115T-65T
160	180									188T-68T
180	200									191T-77T
200	225	-30	44.5T-14.5L	54T-41	63T-41	67T-171	76T-171	90T-31T	109T-50T	130T-77T
225	250									139T-80T
250	280									163T-84L
280	315	-35	51T-16L	62T-41	71T-41	78T-201	87T-201	101T-34T	123T-56T	161T-94L
315	355									165T-98T
355	400	-40	58T-18L	69T-41	80T-41	86T-211	97T-211	113T-37T	138T-62T	184T-106T
400	450									190T-104T
450	500	-45	65T-20L	77T-51	89T-41	95T-231	108T-231	125T-40T	153T-68T	211T-126T
										217T-132T

Table for fit on Housing Unit  $\mu\text{m}$

Nominal outside diameter of bearing D (mm)	$\Delta\text{Dmp}$	high	K7	M7	N7	P7	
6	10	0	-8	10T-13L	15T-8L	19T-4L	24T-1L
10	18	0	-8	12T-14L	18T-8L	23T-3L	29T-3L
18	30	0	-9	15T-15L	21T-9L	28T-2L	35T-5L
30	50	0	-11	18T-18L	25T-11L	33T-3L	42T-6L
50	80	0	-13	21T-22L	30T-13L	39T-4L	52T-8L
80	150	0	-15	25T-25L	35T-15L	45T-5L	59T-9L
120	180	0	-18	28T-30L	40T-18L	52T-6L	68T-10L
150	200	0	-25	28T-37L	40T-25L	52T-13L	68T-3L
180	250	0	-30	33T-43L	46T-30L	60T-16L	79T-3L
250	315	0	-35	36T-51L	52T-35L	66T-21L	88T-1L
315	400	0	-40	40T-57L	57T-40L	73T-24L	98T-1L
400	500	0	-45	45T-63L	63T-45L	80T-28L	108T-0

### 10.3 Taper roller bearing -AFBMA recommended fitting practice

#### AFBMA limits & fitting guidelines

Shaft and housing material, geometry, hardness and surface finish must be carefully controlled. Ground shafts should be finished to 1.3 micron Ra or better; for turned shafts a finish of 2.5µm Ra or better; and housing bores should be finished to 4 micron Ra or better.

To avoid shearing aluminum and magnesium housing during bearing installation, steel inserts should be used; alternatively special lubricants may be used for freezing and heating to facilitate assembly. A minimum interference fit is required for aluminum of 0.0010" per inch of diameter, for magnesium of 0.0015" per inch of diameter.

Where bearings are to be pressed onto a hollow shaft, allowance must be considered for contraction of the hollow shaft in order to maintain the desired radial pressure.

The NEI applications engineer should be consulted for proper fitting practice on all special applications. .

#### AFBMA Automotive Tapered Cone Fitting Practice.

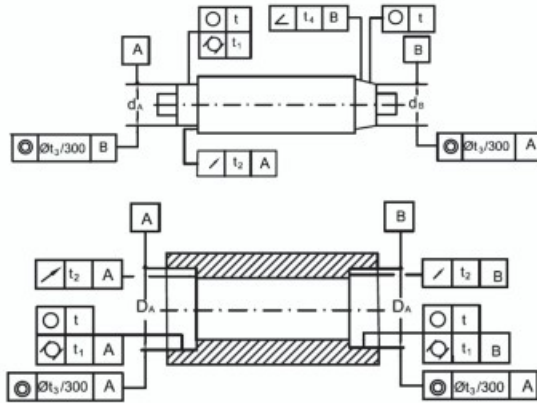
Use	Application	Fit Type	Cone Bore B'	Shaft Diameter B'	Fit	Cone Bore B'	Shaft Diameter B'	Fit
Automotive Rotating Shafts	Pinion, transmission rear wheels, crossshaft, transfer case	Adjustable cones	+0.0005 -0.0000	+0.0005 +0.0000	0.0005L 0.0005L	+0.0010 -0.0000	+0.0015 +0.0005	0.0015T 0.0005T
		Non-Adjustable cones	+0.0005 -0.0000	+0.0015 +0.0010	0.0015T 0.0005T	+0.0010 -0.0000	+0.0025 +0.0015	0.0025T 0.0005T
	Differential	Non-Adjustable cones	+0.0005 -0.0000	+0.0025 +0.0015	0.0025T 0.0010T	+0.0010 -0.0000	+0.0035 +0.0025	0.0035T 0.0015T
Automotive Stationary Shafts	Front wheels, full floating rear wheels trailer wheels	Adjustable cones	+0.0005 -0.0000	-0.0002 -0.0007	0.0002L 0.0012L	+0.0010 -0.0000	-0.0002 -0.0012	0.0002L 0.0022L

#### AFBMA Automotive Tapered Cup Fitting Practice.

Use	Application	Fit Type	Cup O.D. D'	Housing Bore D'	Fit	Cup O.D. D'	Housing Bore D'	Fit	Cup O.D. D'	Housing Bore D'	Fit
			Less 3" O.D.			3" to 5" O.D.			Above 5" O.D.		
Automotive	Front wheels, full floating rear wheels pinion, differential	Non-Adjustable cups	+0.0010 0.0000	-0.0015 -0.0005	0.0025T 0.0005T	+0.0010 -0.0000	+0.0020 +0.0010	0.0030T 0.0010T	+0.0010 -0.0000	-0.0020 -0.0010	0.0040T 0.0010T
		Differential	Non-Adjustable cups	+0.0010 0.0000	+0.0010 +0.0020	0.0000L 0.0020L	+0.0010 -0.0000	+0.0010 +0.0020	0.0000L 0.0020L	+0.0010 -0.0000	-0.0020 -0.0020
	Rear wheels, transmission, cross shaft & other application	Adjustable cups	+0.0010 0.0000	-0.0000 +0.0010	0.0010T 0.0010L	-0.0000 -0.0000	+0.0000 +0.0010	0.0010T 0.0010L	+0.0010 -0.0000	-0.0000 -0.0020	0.0010T 0.0020L

\*D - Normal cup O.D., L - Loose, T - Tight

## 10.4 Shaft and housing accuracies



Tolerance name	Fit	Symbol of deviation	Permissible deviation depending on the tolerance class				
			P0-P6K	P6	P5	P4(SP)	P2(U,P)
Tolerance of dimension	shaft	-	IT6(IT5)	IT5	IT4	IT4	IT3
	housing	-	IT7(IT6)	IT6	IT5	IT4	IT4
Tolerance of roundness and cylindricity	shaft	t, t <sub>1</sub>	$\frac{IT4}{2}$ ( $\frac{IT3}{2}$ )	$\frac{IT3}{2}$ ( $\frac{IT2}{2}$ )	$\frac{IT2}{2}$	$\frac{IT1}{2}$	$\frac{IT0}{2}$
	housing	t, t <sub>1</sub>	$\frac{IT5}{2}$ ( $\frac{IT4}{2}$ )	$\frac{IT4}{2}$ ( $\frac{IT3}{2}$ )	$\frac{IT3}{2}$	$\frac{IT2}{2}$	$\frac{IT1}{2}$
Tolerance of face runout	shaft	t <sub>r</sub>	IT4 (IT3)	IT3 (IT2)	IT2	IT1	IT0
	housing	t <sub>r</sub>	IT5 (IT4)	IT4 (IT3)	IT2	IT2	IT1
Tolerance of concentricity	shaft	t <sub>c</sub>	-	-	-	-	-
Tolerance of angularity	shaft	<	t <sub>c</sub>	t <sub>c</sub>	t <sub>c</sub>	t <sub>c</sub>	t <sub>c</sub>
	housing	-	-	-	-	-	-

For IT grade values refer table for ISO tolerance grade.

Table: ISO Tolerance grade for dimensions

Nominal Dimension Over Incl.	Tolerance Grade																		
	IT0	IT1	IT2	IT3	IT4	IT5	IT6	IT7	IT8	IT9	IT10	IT11	IT12						
mm	μm																		
1	3	0.5	0.8	1.2	2	3	4	6	10	14	25	40	60	100					
3	6	0.6	1	1.5	2.5	4	5	8	12	18	30	48	75	120					
6	10	0.6	1	1.5	2.5	4	6	9	15	22	36	58	90	150					
10	18	0.8	1.2	2	3	5	8	11	18	27	43	70	110	180					
18	30	1	1.5	2.5	4	6	9	13	21	33	52	84	130	210					
30	50	1	1.5	2.5	4	7	11	16	25	39	62	100	160	250					
50	80	1.2	2	3	5	8	13	19	30	46	74	120	190	300					
80	120	1.5	2.5	4	6	10	15	22	35	54	87	140	220	350					
120	180	2	3.5	5	8	12	18	25	40	63	100	160	250	400					
180	250	3	4.5	7	10	14	20	29	46	72	115	185	290	460					
250	315	4	6	8	12	16	23	32	52	81	130	210	320	520					
315	400	5	7	9	13	18	25	36	57	89	140	230	360	570					
400	500	6	8	10	15	20	27	40	63	97	155	250	400	630					
500	630	-	-	-	-	-	28	44	70	110	175	280	440	700					
630	800	-	-	-	-	-	35	50	80	125	200	320	500	800					
800	1000	-	-	-	-	-	36	56	90	140	230	360	560	900					
1000	1250	-	-	-	-	-	42	66	105	165	260	420	660	1050					
1250	1600	-	-	-	-	-	50	78	125	195	310	500	780	1250					
1600	2000	-	-	-	-	-	60	92	150	230	370	600	920	1500					
2000	2500	-	-	-	-	-	70	110	175	280	440	700	1100	1750					